

ME 599/699 Robot Modeling & Control

Fall 2021

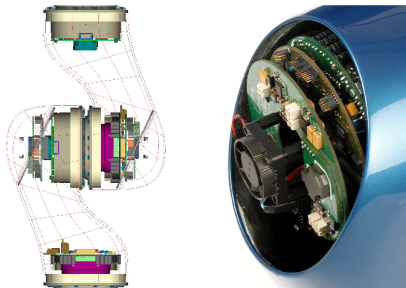
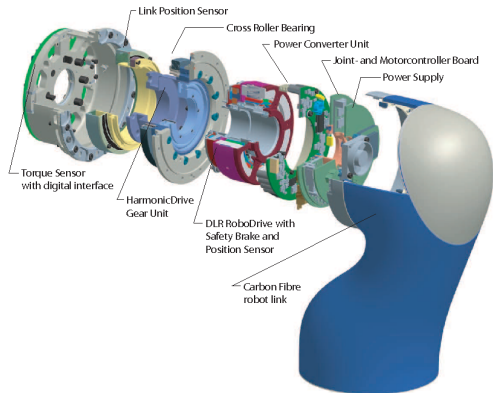
Drive Trains

Hasan A. Poonawala

Department of Mechanical Engineering
University of Kentucky

Email: hasan.poonawala@uky.edu

Web: <https://www.engr.uky.edu/~hap>



Permanent Magnet DC motors

We consider permanent magnet DC motors. Other kinds include AC motors and brushless DC motors.

A model for the motor torque is $\tau = K_m i_a$, if the flux in the motor is constant. The current is generated by a voltage source, and has dynamics

$$L \frac{d}{dt} i_a + R i_a = V - V_b, \quad (1)$$

where L is the motor inductance, R is the winding resistance, V_b is the back EMF and is proportional to ω_m , the motor speed.

PMDC Model

The dynamics governing θ_m are

$$J_m \ddot{\theta}_m + B_m \dot{\theta}_m = \tau_m - \tau_l / r \quad (2)$$

$$= K_m i_a - \tau_l / r \quad (3)$$

We can rewrite (1) and (5) as

$$(Ls + R)I_a(s) = V(s) - K_b s\Theta_m(s), \quad (4)$$

$$(J_ms^2 + B_ms)\Theta_m(s) = K_m I_a(s) - \tau_l(s)/r \quad (5)$$

We combine these equations to obtain

$$s((Ls + R)(J_ms + B_m) + K_b K_m)\Theta_m(s) = K_m V(s) - \frac{(Ls + R)}{r} \tau_l(s). \quad (6)$$

Fast Electrical Dynamics

The electrical time constant L/R is much smaller than the mechanical time constant J_m/B_m . So, we can divide by R and set L/R to zero, obtaining.

$$s \left((J_m s + B_m) + \frac{K_b K_m}{R} \right) \Theta_m(s) = \frac{K_m}{R} V(s) - \frac{1}{r} \tau_l(s).$$

Setting $u \leftarrow K_m V/R$, and $B \leftarrow B_m + K_b K_m/R$, we obtain the motor equation as

$$J \ddot{\theta}_m + B \dot{\theta}_m = u(t) - \frac{1}{r} \tau_l. \quad (7)$$

Combined Link-Actuator Model

Let's combine the motor m with the link l

$$J_m \ddot{\theta}_m + B \dot{\theta}_m = u(t) - \frac{1}{r} \tau_l \quad (8)$$

$$J_l \ddot{\theta}_l + B_l \dot{\theta}_l = \tau_l \quad (9)$$

Due to the gears, $\dot{\theta}_m = r \dot{\theta}_l$. We eliminate θ_l to obtain

$$(J_m r^2 + J_l) \ddot{\theta}_l + (B r^2 + B_l) \dot{\theta}_l = r u \quad (10)$$

Main takeaway: When gear ratio r is large, then link inertia becomes negligible compared to the motor's inertia.

Full Euler-Lagrangian Model

$$D(q)\ddot{q} + C(q, \dot{q})\dot{q} + G(q) = \tau + \tau_{friction} + \tau_e,$$

becomes

$$\underbrace{M(q)}_{\text{+motor inertia}} \ddot{q} + C(q, \dot{q})\dot{q} + \underbrace{B\dot{q}}_{\text{+motor friction}} + G(q) = u + \tau_e,$$

where u denotes the input due to the voltage, whereas τ was the torque acting on the link joint.

Full Euler-Lagrangian Model

$$D(q)\ddot{q} + C(q, \dot{q})\dot{q} + G(q) = \tau + \tau_{friction} + \tau_e,$$

becomes

$$\underbrace{M(q)}_{\text{+motor inertia}} \ddot{q} + C(q, \dot{q})\dot{q} + \underbrace{B\dot{q}}_{\text{+motor friction}} + G(q) = u + \tau_e,$$

where u denotes the input due to the voltage, whereas τ was the torque acting on the link joint. In particular,

$$u_k = r_k \frac{K_{m_k}}{R_k} V_k,$$

where $\theta_{m_k} = r_k q_k$, and $M(q) = D(q) + J$, and J is diagonal with $r_k^2 J_{m_k}$ as k^{th} diagonal element.

Implications of PMDC Motors

- ▶ The gear ratio is high ($\approx 20 - 200$),
 J dominates $D(q)$ and other terms

Implications of PMDC Motors

- ▶ The gear ratio is high ($\approx 20 - 200$),
 J dominates $D(q)$ and other terms
 - ▶ $\implies M(q) \approx \text{diagonal}$, dynamics of links nearly independent

Implications of PMDC Motors

- ▶ The gear ratio is high ($\approx 20 - 200$),
 J dominates $D(q)$ and other terms
 - ▶ $\implies M(q) \approx$ diagonal, dynamics of links nearly independent
- ▶ High gear ratios are good for position control

Implications of PMDC Motors

- ▶ The gear ratio is high ($\approx 20 - 200$),
 J dominates $D(q)$ and other terms
 - ▶ $\implies M(q) \approx$ diagonal, dynamics of links nearly independent
- ▶ High gear ratios are good for position control
- ▶ They amplify nonlinear motor friction, introduce friction

Implications of PMDC Motors

- ▶ The gear ratio is high ($\approx 20 - 200$), J dominates $D(q)$ and other terms
 - ▶ $\implies M(q) \approx$ diagonal, dynamics of links nearly independent
- ▶ High gear ratios are good for position control
- ▶ They amplify nonlinear motor friction, introduce friction
 - ▶ the relationship $\tau = K I = KV/R$ breaks down (cannot set torque without feedback)

Implications of PMDC Motors

- ▶ The gear ratio is high ($\approx 20 - 200$), J dominates $D(q)$ and other terms
 - ▶ $\implies M(q) \approx$ diagonal, dynamics of links nearly independent
- ▶ High gear ratios are good for position control
- ▶ They amplify nonlinear motor friction, introduce friction
 - ▶ the relationship $\tau = K I = KV/R$ breaks down (cannot set torque without feedback)
- ▶ In dynamic robots, preference for Direct-Drive and Quasi-Direct-Drive motors ($r \approx 1$)

Implications of PMDC Motors

- ▶ The gear ratio is high ($\approx 20 - 200$), J dominates $D(q)$ and other terms
 - ▶ $\implies M(q) \approx$ diagonal, dynamics of links nearly independent
- ▶ High gear ratios are good for position control
- ▶ They amplify nonlinear motor friction, introduce friction
 - ▶ the relationship $\tau = K I = KV/R$ breaks down (cannot set torque without feedback)
- ▶ In dynamic robots, preference for Direct-Drive and Quasi-Direct-Drive motors ($r \approx 1$)
 - ▶ Brushless, QDD Motors, instrumental in 4-legged bots

Implications of PMDC Motors

- ▶ The gear ratio is high ($\approx 20 - 200$), J dominates $D(q)$ and other terms
 - ▶ $\implies M(q) \approx$ diagonal, dynamics of links nearly independent
- ▶ High gear ratios are good for position control
- ▶ They amplify nonlinear motor friction, introduce friction
 - ▶ the relationship $\tau = K I = KV/R$ breaks down (cannot set torque without feedback)
- ▶ In dynamic robots, preference for Direct-Drive and Quasi-Direct-Drive motors ($r \approx 1$)
 - ▶ Brushless, QDD Motors, instrumental in 4-legged bots
- ▶ Boston Dynamics' Atlas robot uses hydraulic actuation