## 1 Stability Of A System

Consider the simple pendulum at its downward position, with zero velocity. The ouput is the angle $\theta$, which is zero as shown


Figure 1: Pendulum in downward equilibrium position.
A quick sidewards tap on the mass is known as providing an impulse. We're sure that the pendulum moves away from the downward position in response to the tap. But what will happen in the long run? Here, we're asking for the impulse response of the simple pendulum.

For any input or initial conditions, there are three possible behaviors of the impulse response $y_{i}(t)=\mathcal{L}^{-1}\{G(s)\}$ :

1. $y_{i}(t)$ is unbounded $\left(\left|y_{i}(t)\right| \rightarrow \infty\right)$
2. $y_{i}(t)$ is bounded (We can find $0<M<\infty$ such that $\left|y_{i}(t)\right| \leq M$ for all $\left.t\right)$
3. $\lim _{t \rightarrow \infty} y_{i}(t)=0$

We can use these three behaviors to define three notions of stability:

Definition 1 (Unstable). $G(s)$ is unstable (US) if its impulse response is unbounded.

Definition 2 (Lyapunov Stable). $G(s)$ is Lyapunov stable (LS) if its impulse response is bounded.

Definition 3 (Asymptotically Stable). $G(s)$ is asymptotically stable (AS) if its impulse response satisfies $\lim _{t \rightarrow \infty} y_{i}(t)=0$.

Note: An asymptotically stable TF is Lyapunov stable. An unstable system is not LS, and therefore not AS either.

Remark: Why are we interested in $y_{i}(t) \rightarrow 0$ instead of $y_{i}(t) \rightarrow a$, where $a \neq 0$ ? The answer is that we assume we are interested in equilibria, and for a linear system, 0 is its equilibrium.

### 1.1 Stability and Poles of the Transfer Func- Fact: G(s) is unstable (US) if has a pole tion <br> - in the open right half plane (OHRP), or

Let's apply the notion of multiplicity of roots, first mentioned in Laplace transforms, to the multiplicity of poles.

Definition 4 (Multiplicity). Let $G(s)=\beta(s) / \alpha(s)$. If $\alpha(p)=0$,

$$
\lim _{s \rightarrow p} \frac{\alpha(s)}{(s-p)^{n}} \neq 0, \text { and } \lim _{s \rightarrow p} \frac{\alpha(s)}{(s-p)^{n-1}}=0
$$

then $p$ is a pole of $G(s)$ with multiplicity $n$.
Example 1. Let

$$
G(s)=\frac{1}{(s-2)(s-1)^{2} s^{3}}
$$

Now, $\alpha(s)=(s-2)(s-1)^{2} s^{3}$. By our definition above,

- $p_{1}=2$ is a pole of $G(s)$ with multiplicity 1
- $p_{2}=1$ is a pole with multiplicity 2
- $p_{3}=0$ is a pole with multiplicity 3

Fact: $G(s)$ is asymptotically stable (AS) if and only if all its poles are in the open left half plane (OLHP).

Fact: $G(s)$ is Lyapunov stable (LS) if all its poles either

- are in the OLHP, or
- are on the imaginary axis (IA) with multiplicity 1.
- on the IA with multiplicity greater than 1.

These facts above are one example of the idea studying $G(s)$ tells us something about the responses of a system to a given set of inputs.
Example 2. Consider a system with transfer function $G(s)$ given by

$$
\begin{equation*}
G(s)=\frac{s}{s^{2}+5 s+6} \tag{1}
\end{equation*}
$$

Classify the stability properties of this sytem.
Solution: The denominator polynomial is $s^{2}+5 s+6$. The poles of $G(s)$ are therefore the solutions (or, roots) of the equation $s^{2}+5 s+6=0$, which turn out to be $p_{1}=-2, p_{2}=-3$ (we can also say $p_{1}=-3, p_{2}=-2$ ). The real part of both these roots are in the OLHP, therefore $G(s)$ is asymptotically stable. Since $G(s)$ is asymptotically stable (AS), it is also Lyapunov stable (LS).

Example 3. Consider a system with transfer function $G(s)$ given by

$$
\begin{equation*}
G(s)=\frac{s}{s^{2}-6 s+5} \tag{2}
\end{equation*}
$$

Classify the stability properties of this sytem.
Solution: The denominator polynomial is $s^{2}-6 s+5$. The poles of $G(s)$ are therefore the solutions (or, roots) of the equation $s^{2}-6 s+5=0$, which turn out to be the complex conjugate pair $p_{1,2}=3 \pm j 2$. The real part of both these roots are strictly positive, the poles are in the ORHP, therefore $G(s)$ is unstable (US).

### 1.2 Initial and Final Value Theorems

In some case, we may only want to know the value of $y(t)$ at specific times of interest, and solving for $y(t)$ using the inverse Laplace transform is involved. For example, consider a system that is stable, but not asymptotically stable. Then, $y(t)$ remains bounded, and if it approaches a constant value, we'd like to know what that value is. We may be able to calculate this value without ever solving for $y(t)$. The Final Value Theorem helps us do this.

### 1.2.1 Final Value Theorem

Let $y(t)$ have the Laplace transform $\hat{y}(s)$ (which could be a response of the form $G(s) \hat{u}(s))$. If the poles of $\hat{y}(s)$ are in the OLHP with the possible exception of a single pole at zero. Then,

$$
\begin{equation*}
\lim _{t \rightarrow \infty} y(t)=\lim _{s \rightarrow 0} s \hat{y}(s) . \tag{3}
\end{equation*}
$$

### 1.2.2 Initial Value Theorem

A similar result let's us know what the initial value is.

$$
\begin{equation*}
y(0)=\lim _{t \rightarrow 0} y(t)=\lim _{s \rightarrow \infty} s \hat{y}(s) . \tag{4}
\end{equation*}
$$

Example 4. Consider the response of a second order system to a step input:

$$
\hat{y}_{\text {step }}(s)=\frac{\omega_{n}^{2}}{s\left(s^{2}+2 \xi \omega_{n} s+\omega_{n}^{2}\right)}
$$

where $\xi>0$ Find the initial and final value of the response.

## Solution:

$$
\begin{align*}
y_{\text {step }}(0) & =\lim _{s \rightarrow \infty} s \hat{y}_{\text {step }}(s)  \tag{5}\\
& =\lim _{s \rightarrow \infty} s \frac{\omega_{n}^{2}}{s\left(s^{2}+2 \xi \omega_{n} s+\omega_{n}^{2}\right)}  \tag{6}\\
& =\lim _{s \rightarrow \infty} \frac{\omega_{n}^{2}}{s^{2}+2 \xi \omega_{n} s+\omega_{n}^{2}}  \tag{7}\\
& =0 \tag{8}
\end{align*}
$$

Since $\xi>0$, two poles are in the open left half plane, and one on the imaginary axis. Therefore, we may use the FVT to calcluate $y_{\text {step }}(\infty)$.

$$
\begin{align*}
y_{\text {step }}(\infty) & =\lim _{s \rightarrow 0} s \hat{y}(s)  \tag{9}\\
& =\lim _{s \rightarrow 0} s \frac{\omega_{n}^{2}}{s\left(s^{2}+2 \xi \omega_{n} s+\omega_{n}^{2}\right)}  \tag{10}\\
& =\lim _{s \rightarrow 0} \frac{\omega_{n}^{2}}{s^{2}+2 \xi \omega_{n} s+\omega_{n}^{2}}  \tag{11}\\
& =1 \tag{12}
\end{align*}
$$

If we have a mass-spring-damper at equilibrium, and apply a step input force $f(t)$ on the mass, the response of the position of the mass $y=q$ is

$$
\begin{equation*}
\hat{y}(s)=\frac{1}{\left(m s^{2}+c s+k\right)} \frac{1}{s} \Longrightarrow y_{\text {step }}(\infty)=\frac{1}{k} \tag{13}
\end{equation*}
$$

We've just shown that a stiffer spring (higher $k$ ) reduces the distance (smaller $1 / k$ ) by which a constant force (step input $f(t))$ moves the resting position $\left(0 \rightarrow \frac{1}{k}\right)$.

